From Triangulation to Simplex Mesh: a Simple and Efficient Transformation

Francisco J. GALDAMES[a,c], Fabrice JAILLET[b,c]

(a) Department of Electrical Engineering, Universidad de Chile, Av. Tupper 2007, Santiago, Chile

(b) Université de Lyon, IUT Lyon 1, Département Informatique, F-01000, France

(c) Université de Lyon, CNRS, Université Lyon 1, LIRIS, équipe SAARA, UMR5205, F-69622, France

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Abstract

In the field of 3D images, relevant information can be difficult to interpret without further computer-aided processing. Generally, and this is particularly true in medical imaging, a segmentation process is run and coupled with a visualization of the delineated structures to help understanding the underlying information. To achieve the extraction of the boundary structures, deformable models are frequently used tools. Amongst all techniques, Simplex Meshes are valuable models thanks to their good propensity to handle a large variety of shape alterations altogether with a fine resolution and stability. However, despite all these great characteristics, Simplex Meshes are lacking to cope satisfyingly with other related tasks, as rendering, mechanical simulation or reconstruction from iso-surfaces. As a consequence, Triangulation Meshes are often preferred. In order to face this problem, we propose an accurate method to shift from a model to another, and conversely. For this, we are taking advantage of the fact that triangulation and simplex meshes are topologically duals, turning it into a natural swap between these two models. A difficulty arise as they are not geometrically equivalent, leading to loss of information and to geometry deterioration whenever a transformation between these dual meshes takes place. Therefore, some effort as to be carried out to minimizing the shape degradation using an appropriate interpolation to find the position of the vertices in the dual mesh. An accurate and effective transformation technique is described in this paper, where we present a direct method to perform an interpolation of a simplex mesh to obtain its dual, and/or vice-versa. This original method is based on the distance minimization between the tangent planes of the mesh and vertices of each face. Finally, probing resulting mesh shiftings in both directions are commented.

Keywords: Simplex mesh; triangulation mesh; optimized surface interpolation; surface mesh transformation

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Introduction

Deformable model techniques are widely used in image segmentation tasks. Among these models, it is indubitable that simplex meshes are valuable candidates [3], for their favorable characteristics in this type of modeling, as its easy control and convenient way to model internal forces. With this type of meshes, as with triangulations, any topology can be described. Furthermore, simplex meshes and triangulations are topologically duals, and this allows us to naturally obtain a simplex mesh by applying a dual operation to the triangulation, and vice versa. On the other hand, very efficient algorithms exist to generate triangulations from a given geometry [9, 6], while this can be more arduous using simplex meshes. So, in some cases it could be appropriate to generate first a triangulation (from an isosurface, for example), and next to transform this latter into a simplex mesh, with the intention to controlling the deformation of the model [10].

Moreover, for many applications, simplex meshes are not suitable and triangulated meshes are required. For example, there are different meshing methods to generate inner tetrahedral or hexahedral elements [7], but in general they need as input a surface representation that clearly defines the geometry, with planar faces and without self-intersections between elements. Piecewise linear complex (PLC) [1] and triangulation are eligibles. However, simplex meshes do not meet these requirements since faces are not necessarily planar. One possibility would be to transform the simplex mesh into a triangulation before creating the volumetric mesh. Rendering and calculation of area, may be other tasks where it is preferable to handle triangulations instead of simplex meshes.

Triangulations and simplex meshes are topologically duals, but not geometrically equivalents [3]. It is not possible to build a homeomorphism between the set of coordinates of a triangulation and the one of its dual simplex mesh. Therefore, there is loss of information and geometry deterioration whenever a transformation between these meshes takes place. Currently, the most common way to perform this transformation is to determine the set of vertices for the final mesh as the gravity center of each face of the initial mesh. However, in this case, mesh softening is very high; original shape (curvature) and volume is far to be accurately respected. An alternative to transform a simplex mesh into a triangulation, is to compute the gravity center of each face and next insert this point with the other face vertices before to perform a triangulation. Although this method reduces the geometry deterioration, the resulting mesh is not dual to the initial simplex mesh, and moreover, the number of points will rise considerably. It is also possible to consider only the face vertices, but the resulting mesh is either not topologically dual. Moreover, the converse process to obtain a simplex mesh from a triangulation is not straightforward. For all these reasons, it is useful to have a proper method to perform transformations between these two types of meshes with minimal loss of information, that is the purpose of this paper.

From a geometric point of view, the problem can be reduced to find an interpolation of the center of each face, and to build the dual mesh accordingly

to these points. Subdivision, variational surfaces, traditional splines or implicit surfaces are amongst the most used techniques to find interpolating points in a mesh. As the requirement here is to get a simple and straightforward method, we have chosen a geometric interpolation, based on the distance to the tangent planes of the points of each face. A similar measure has been successfully used in [8] to compute a local geometric error based on the maximal distance to a set of planes, in order to perform triangular mesh simplifications. In an equivalent work, a similar measure has been employed, but this time a summation was used to obtain a quadratic error [4, 5]. In a more recent work, a method for refining triangulations has been developed [11]. It is based on face splitting and interpolation using distance minimization over the neighboring triangles planes. Here, it is worth to notify that our global objective is to perform a transformation between meshes, and not to refine them. However, we mainly got inspiration from this last work, but in our case the error measurement is applied to find the points of a dual mesh, to permit shifting between simplex meshes and triangulations, and conversely.

The paper is organized as follows. In section 1, we present essential background on simplex meshes, their characteristics and relationship with triangulations. The main part concerning the interpolation method used to find the dual mesh is explained in section 2. Application of this method to swap between meshes is shown in sections 3 and 4, where details can be found for each swap direction. Finally, some results are exhibited in section 5, followed by conclusions in 6.

1 Triangulation vs. simplex mesh

As stated in the introduction, a simplex mesh can be seen as the topological dual of a triangulation, each vertex of the simplex mesh corresponds to a triangle in the corresponding dual triangulation (Fig. 1). However, simplex meshes and triangulations are not geometrically duals. Their geometry is determined by the coordinates of their vertices; nevertheless, the number of vertices is different between a simplex V_{SM} and a triangulation V_{TM}. The Euler's characteristic for a triangulations without holes and its dual simplex mesh states:

$$V_{TM} - \frac{V_{SM}}{2} = 2(1 - g), \tag{1}$$

where g is the genus of the mesh. As the sets of coordinates have different dimensions for a triangulation and its dual simplex mesh, no homomorphism can be constructed between them.

Simplex meshes are privileged candidates to be used in segmentation methods based on deformable models. Each vertex of a simplex mesh has three neighbors; between them, a restricted number of entities is defined, the simplex angle and the metric parameters. The simplex angle ρ_i is defined for each vertex p_i by means of its neighborhood $p_{N1(i)}, p_{N2(i)}, p_{N3(i)}$. The normal vector to the plane defined by the three neighbors $\overrightarrow{N_i}$, the circle of center C_i and radius r_i
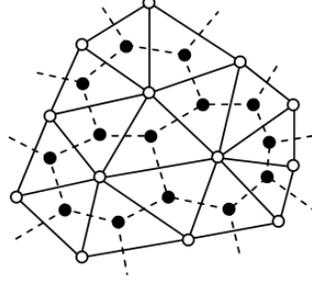
Figure 1: Simplex meshes and triangulations are topological but not geometrical duals. White dots: triangulation vertices ; Black dots: simplex mesh vertices.

defined by these neighbors, and the sphere of center O_i and radius R_i defined by the four vertices can easily be extracted from topology. Thus, the simplex angle can be defined as (Fig.2):

$$\rho \in [-\pi, \pi]$$
$$sin(\rho_i) = \frac{r_i}{R_i} sign\left(\overrightarrow{p_i p_{N1(i)}} \cdot \overrightarrow{N_i}\right)$$
$$cos(\rho_i) = \frac{\|O_i C_i\|}{R_i} sign\left(\overrightarrow{O_i C_i} \cdot \overrightarrow{N_i}\right) \tag{2}$$

The simplex angle can be considered as a measure of the height of vertex p_i with
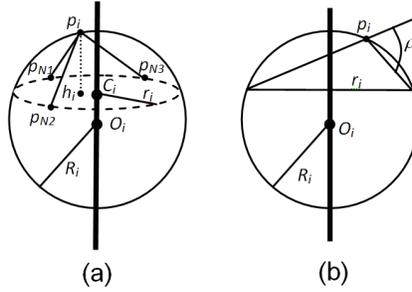

(a)   (b)

Figure 2: a) Tetrahedron formed by point p_i and its 3 neighbors $p_{N1(i)}, p_{N2(i)}, p_{N3(i)}$, with the circle defined by the neighbors, and the sphere containing those four points. b) Projection on a plane passing through O_i, C_i and p_i, revealing the simplex angle.

respect to the plane defined by its neighbors. The metric parameters $\varepsilon_{1i}, \varepsilon_{2i}, \varepsilon_{3i}$ describe the relative position of a vertex according to its neighbors. The position of the projection h_i of vertex p_i on the plane defined by its neighbors (Fig. 2)

can be expressed as:

$$h_i = \varepsilon_{1i} p_{N1(i)} + \varepsilon_{2i} p_{N2(i)} + \varepsilon_{3i} p_{N3(i)}$$
$$\varepsilon_{1i} + \varepsilon_{2i} + \varepsilon_{3i} = 1 \tag{3}$$

Thus, the metric parameters ε_i and the simplex angle ρ_i completely determine the position of a vertex in the following way:

$$p_i = h_i + L(r_i, d_i, \rho_i)\overrightarrow{N_i}, \tag{4}$$

where $d_i = |C_i - h_i|$, and L is defined as:

$$L(r_i, d_i, \rho_i) = \frac{(r_i^2 - d_i^2)tan(\rho_i)}{\chi\sqrt{r_i^2 + (r_i^2 - d_i^2)tan^2(\rho_i)} + r_i}$$
$$\chi = \begin{cases} 1 & \text{if } |\rho_i| < \pi/2 \\ -1 & \text{if } |\rho_i| > \pi/2 \end{cases} \tag{5}$$

To perform transformations in any direction between these two types of dual meshes, we have to find an associated point q_u of the dual mesh M_2 for each face f_u of the initial mesh M_1. When dealing with triangulations, faces are triangles; and conversely for simplex meshes, faces are polygons whose vertices are generally not coplanar. The resulting mesh M_2 should have a regular shape and preserve the geometry defined by M_1, what is far from being straightforward. Trying to keep the geometry, we can impose q_u being close to the tangent planes π_i of each summit p_i defining the face f_u. Constraining M_2 to have a regular shape, can be achieved by choosing q_u close to the center of the face f_u, i.e. minimize the distance between q_u and all p_i. Therefore, we must minimize the distance between a point q_u and a set of points and planes. Accordingly, the present method tries to compensate the lack of existing techniques on these aspects.

2 Interpolation based on tangent planes

The equation of a plane can be denoted as $A \cdot p = 0$, where $A = [a, b, c, d]$ and $p = [x_p, y_p, z_p, 1]^T$ is a point lying on this plane. The coefficients a, b, c are the components of the unit vector $\overrightarrow{N}$ normal to the plane, and $d = -\overrightarrow{N} \cdot p$. For q an arbitrary point of the space, $|A \cdot q|$ is the distance to the plane.

Considering now a set of planes π_i represented by $A_i \cdot p = 0$ $(i = 1, \ldots, L)$, the distance between any point $q = [x, y, z, 1]^T$ to each plane π_i is $|A_i \cdot q|$. On the other hand, let's consider a set of points p_j $(j = 1, \ldots, M)$. If we want to find the point q minimizing its distance to planes π_i and points p_j, the function to be considered follows:

$$D(q) = \sum_{i=1}^{L} \alpha_i |A_i \cdot q|^2 + \sum_{j=1}^{M} \beta_j |q - p_j|^2 \tag{6}$$

where α_i and β_j are the weights for the distance to the planes (in order to respect geometry and curvature) and points (controlling shape regularity), respectively. Equation (6) can be rewritten in matrix form as:

$$D(q) = q^T Q q \tag{7}$$

where

$$Q = \sum_{i=1}^{L} \alpha_i A_i^T A_i + \sum_{j=1}^{M} \beta_j Q_j \tag{8}$$

and

$$Q_j = \begin{bmatrix} 1 & 0 & 0 & -x_j \\ 0 & 1 & 0 & -y_j \\ 0 & 0 & 1 & -z_j \\ -x_j & -y_j & -z_j & x_j^2 + y_j^2 + z_j^2 \end{bmatrix} \tag{9}$$

Since Q_j and $A_i^T A_i$ are symmetric matrices, then Q is also symmetric and can be written as:

$$Q = \begin{bmatrix} q_{11} & q_{12} & q_{13} & q_{14} \\ q_{12} & q_{22} & q_{23} & q_{24} \\ q_{13} & q_{23} & q_{33} & q_{34} \\ q_{14} & q_{24} & q_{34} & q_{44} \end{bmatrix} \tag{10}$$

To minimize the quadratic form of eq. (7), let's solve the following system of equations:

$$\frac{\partial D(q)}{\partial x} = 0, \ \frac{\partial D(q)}{\partial y} = 0, \ \frac{\partial D(q)}{\partial z} = 0. \tag{11}$$

Taking the partial derivatives of:

$$q^T Q q = q_{11}x^2 + 2q_{12}xy + 2q_{13}xz + 2q_{14}x + q_{22}y^2$$
$$+ 2q_{23}yx + 2q_{24}y + q_{33}z^2 + 2q_{34}z + q_{44}, \tag{12}$$

it can be noticed that the system in eq. (11) can be rewritten in a matrix form as:

$$\begin{bmatrix} q_{11} & q_{12} & q_{13} & q_{14} \\ q_{12} & q_{22} & q_{23} & q_{24} \\ q_{13} & q_{23} & q_{33} & q_{34} \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} x \\ y \\ z \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} \tag{13}$$

Finally, the solution of eq. (13) follows:

$$\begin{bmatrix} x \\ y \\ z \end{bmatrix} = \begin{bmatrix} q_{11} & q_{12} & q_{13} \\ q_{12} & q_{12} & q_{23} \\ q_{13} & q_{23} & q_{33} \end{bmatrix}^{-1} \begin{bmatrix} -q_{14} \\ -q_{24} \\ -q_{34} \end{bmatrix} \tag{14}$$

where $q = [x, y, z]^T$.

Weights calculation.

The solution of equation (6) can be understood as an affine combination of the generalized intersection of all planes π_i (first term) and the average of all points p_j (second term). This affine combination is controlled by the weights α_i and β_i. For example, let's consider points p_1, p_2 and planes π_1, π_2 as shown on Figure 3. Planes intersect at point p_α, and the average of the points (for $\beta_i = \beta$) is p_β. The weights α_i should reflect the importance of each plane to the interpolation; and this importance will be estimated in a different way for triangulations or simplex meshes, as this will be detailled in the next sections.
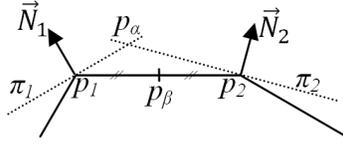

Figure 3: Solution of equation (6) as the affine combination of the generalized intersection of planes π_i (p_α) and the average of all points p_i (p_β, for $\beta_i = \beta$).

The weights β_i can be calculated using an analogue method to the one used for mesh refinement in [11]. We are looking for an interpolated point q at the center of each face. Assuming that points p_i define a face, and $\overrightarrow{N_i}$ are the unit normal vectors to the mesh at p_i, then we can estimate the position for q as:

$$\bar{q} = c_u + w \sum_{i=1}^{L} ((p_i - c_u) \cdot \overrightarrow{N_i}) \overrightarrow{N_i} \tag{15}$$

where w is a free positive parameter controlling the smoothness of the interpolation, and where:

$$c_u = \frac{1}{L} \sum_{i=1}^{L} p_i. \tag{16}$$

Substituting q with this estimation $\bar{q}$ in eq. (13), it follows:

$$\begin{bmatrix} q_{11} & q_{12} & q_{13} & q_{14} \\ q_{12} & q_{22} & q_{23} & q_{24} \\ q_{13} & q_{23} & q_{33} & q_{34} \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \bar{x} \\ \bar{y} \\ \bar{z} \\ 1 \end{bmatrix} = \begin{bmatrix} \delta_x \\ \delta_y \\ \delta_z \\ 1 \end{bmatrix}, \tag{17}$$

Now, the weights β_i that minimize the residues δ should be found, such that $\bar{q}$ approaches the solution of equation (17) for those β_i. As q should lie close to the face center, the same weight can be assigned to all points, $ie.$ $\beta_i = \beta$. Using

the original planes to express the residues δ, it follows:

$$\delta_x = \sum_{i=1}^{L} \alpha_i a_i \left(A_i \cdot \bar{q}\right) + \beta \left(L\bar{x} - \sum_{i=1}^{L} x_i \right)$$

$$\delta_y = \sum_{i=1}^{L} \alpha_i b_i \left(A_i \cdot \bar{q}\right) + \beta \left(L\bar{y} - \sum_{i=1}^{L} y_i \right)$$

$$\delta_z = \sum_{i=1}^{L} \alpha_i c_i \left(A_i \cdot \bar{q}\right) + \beta \left(L\bar{z} - \sum_{i=1}^{L} z_i \right) \tag{18}$$

So, finding the weight β can be achieved by minimizing $\delta_x^2 + \delta_y^2 + \delta_z^2$. The solution of $\partial(\delta_x^2 + \delta_y^2 + \delta_z^2)/\partial\beta = 0$ leads to:

$$\beta = \frac{TB}{B^2} \tag{19}$$

where:

$$T = \sum_{i=1}^{L} \alpha_i (A_i \cdot \bar{q}) \overrightarrow{N_i},$$

$$and\ B = \sum_{i=1}^{L} (p_i) - L\bar{q} \tag{20}$$

3   From triangulation to simplex surface mesh

In this section, we will see the first case, ie. details when performing the mesh transformation from a triangulation to a simplex surface. In this case, an appropriate point q_u on the new simplex mesh must be calculated for each triangular face t_u. Then, we need information for each triangle t_u about the curvature of the mesh. Let us consider the tangent planes to the vertices p_i $(i = 1, 2, 3)$ composing triangle t_u; these planes π_i can be written as $A_i \cdot p = 0$ as defined previously. The normal vectors that define these planes can be calculated as:

$$\overrightarrow{N_i} = \frac{\sum_{k=1}^{L_i} \phi_k \overrightarrow{N_k}}{\left\| \sum_{k=1}^{L_i} \phi_k \overrightarrow{N_k} \right\|}, \tag{21}$$

where $\overrightarrow{N_k}$ $(k = 1, \ldots, L_i)$ are the normals of the triangles t_k to which the vertex p_i belongs, and ϕ_k is the angle of the triangle t_k at vertex p_i (Fig. 4).

To approximate the surface, the distance between the new point q_u and planes π_i is minimized. Again, q_u should not lie too far from the center of triangle t_u to preserve a regular shape, so q_u should minimize its distance to points p_i. As aforementioned, the direct minimization of eq. (6) will provide us an appropriate q_u.
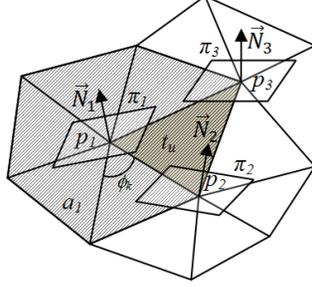
Figure 4: Scheme of triangle t_u, planes and points used to find vertex q_u of the dual simplex mesh.

Each weight α_i is calculated based on the area a_i corresponding to the sum of the areas of all triangles t_k sharing p_i (Fig. 4):

$$\alpha_i = \frac{a_i}{\sum_{j=1}^{3} a_j}. \qquad (22)$$

This way, the distance to each plane is weighted according to the area of triangles that were used to calculate it. The weights β_i are calculated using the same technique as described in section 2, equation (19).

4 From simplex to triangulation surface mesh

In this section, we are dealing now with the converse case. A point q_u of the triangulation must be calculated for each face f_u of the simplex mesh. However, faces of a simplex mesh do not have a fixed number of points p_i ($i = 1, \ldots, N_u$), and moreover they are generally not coplanar. The distance between q_u and the planes π_i tangent to the points p_i, is minimized to maintain the geometry of the mesh. These planes are defined by the points p_i and the normal vector at each point. In a simplex mesh, normals are defined by the plane containing the three neighbors $p_{N1(i)}, p_{N2(i)}, p_{N3(i)}$ (Fig. 2) of the considered point p_i [3]. As in the inverse case, q_u should lie close to the center of the face f_u to preserve a regular shape. Figure 5 illustrates these planes and points. As previously, eq. (6) can be used to calculate q_u by minimizing the distance to planes π_i and points p_i.

The surface of the circle defined by the neighbors at each point p_i is a good estimation of the importance the plane π_i has within the mesh, thus its radius r_i is used to calculate the weights α_i (Fig. 2). It follows:

$$\alpha_i = \frac{r_i^2}{\sum_{i=j}^{N_u} r_j^2} \qquad (23)$$

Again, in this case, weights β_i are calculated using the same technique described in section 2, equation (19).
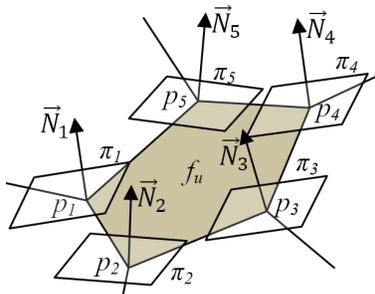
Figure 5: Scheme of face f_u, planes and points used to find vertex q_u of the dual triangulation.

5 Results

When performing a transformation between simplex meshes and triangulations (and conversely), a similar mesh to the original one is expected, in order to produce minimal resultant geometric perturbation. In order to measure the quality of the transformations in both directions, the set of transformations $(TM_1 \rightarrow SM_1 \rightarrow TM_2 \rightarrow \cdots \rightarrow TM_k \rightarrow SM_k \rightarrow TM_{k+1} \rightarrow \cdots \rightarrow TM_N \rightarrow SM_N)$ is performed, where TM_k is a triangulation and SM_k a simplex mesh, with $(k = 1, \ldots, N)$.

The present technique has been compared to the most commonly used at this time, *ie.* using the Center of Mass of each face to compute the corresponding point of the dual mesh [3]. Since all meshes TM_k have the same number of points, idem as the SM_k between them, we have considered that the most appropriate measure was a simple point-to-point distance computation after each transformation cycle. This way, each triangulation is compared at each step to the first triangulation; and correspondingly, each simplex meshes is considered accordingly to the first simplex mesh obtained.

Figure 6 shows the distance graph measured for the surface of cerebral ventricles (1360 points/simplex faces, 2728 triangles/points), for 150 iterations. The point-to-point mean distances are expressed as a percentage of the bounding box diagonal of TM_1 or SM_1 for the triangulation or simplex mesh, respectively. Curve 6(a) shows results using the *Center of Mass* technique, while 6(b) draws results with our original technique. If we compare the results for a set of meshes, the *Center of Mass* technique produces high degeneration in some parts of the mesh (Fig. 7(b), (d) and (f)), losing most of the details present in the initial geometry. However, using an interpolation based on the tangent planes as presented in this article, it can clearly be seen on Fig. 7(c), (e) and (g), that the initial geometry is much better preserved.

As a complementary result, the Hausdorff distance was measured as well between initial and transformed meshes by using the `Metro` tool that adopts a surface sampling approach [2]. The *Prism* (92 vertices, 180 triangles; *from AIM@SHAPE*), *Block*(2132 vertices, 4272 triangles; from *AIM@SHAPE*), *Horse*
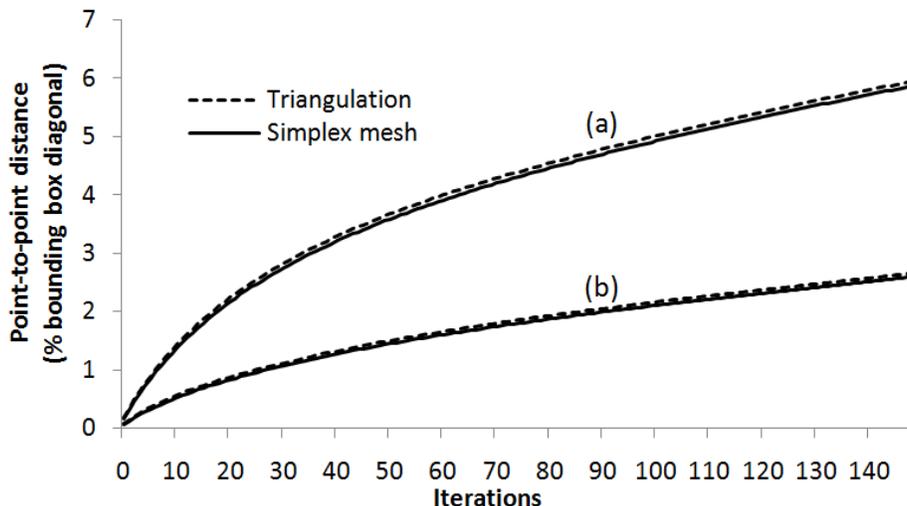
Figure 6: Curves of the mean error of the successive transformations of a cerebral ventricles surface (a) Transformation based on the faces center of mass. (b) Interpolation based on tangent planes.

(48485 vertices, 96966 triangles; from *Cyberware, Inc*), and *Bunny* (34834 vertices, 69451 triangles; from *Stanford 3D Scanning Repository*) meshes have been considered; and the distance was measured after a cycle of transformations, i.e. swapping to simplex mesh and back to triangulation. Figure 8 shows the initial mesh with coloration according to this distance to the resulting one, and Table 1 shows the well known ratio between measured distances and the bounding box diagonal of the original mesh. The mean and RMS distances between two surfaces M_1 and M_2 are defined as:

$$\text{Mean distance}(M_1, M_2) = \frac{1}{|M_1|} \int_{p \in M_1} \text{HD}(p, M_2) ds$$

$$\text{RMS distance}(M_1, M_2) = \sqrt{\frac{1}{|M_1|} \int_{p \in M_1} \text{HD}(p, M_2)^2 ds},$$

were $\text{HD}(p, M)$ is the Hausdorff distance between point p and surface M, and $|M|$ is the area of M. The computation time was multiplied by approximately 30 with our method; eg. the computation time for the prism mesh was 0.007161 with the center of mass and 0.270000 seconds with our method [1]. As it can be guessed, in both cases, the main error is concentrated in high curvature areas. But, as previously seen, the error dramatically decreases with our technique (Fig. 8, right column) compared to the *Center of Mass* (left column).

Figure 9 shows a comparison between the initial (darker) and the resulting (lighter) meshes, using both methods. Errors are significantly lower in our case

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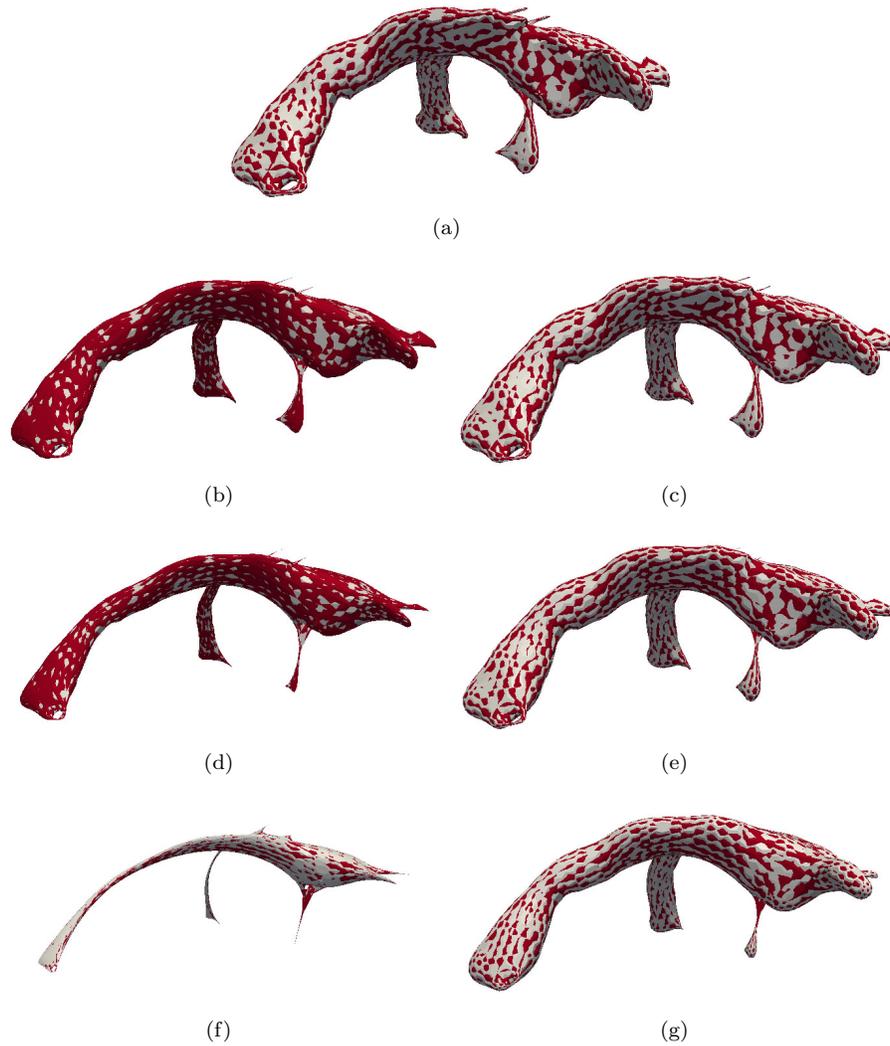[1] developed in Python Language on AMD Athlon 62x2 Dual, 2GHz, 1Gb RAM

Figure 7: Cerebral ventricles mesh after successive transformations between simplex (lighter) mesh and triangulation (darker). Left: meshes obtained using the faces' mass centers, after (b) 5 , (d) 15 and (f) 50 cycles. Right: meshes obtained using our technique, after (c) 5, (e) 15 and (g) 50 cycles.

(b) than for the *Center of Mass* technique (a). Moreover, the resulting mesh tends to be inside (resp. outside) the initial mesh in areas with positive (resp. negative) curvature for the classic technique, while our technique avoids this construction artifact, thanks to the introduction of an appropriate weighting between element regularity and surface smoothness.

Table 1: Hausdorff distances.

		Center of Mass	Distance to Planes	Gain [%]
Prism Mesh	min	0,003537	0,000016	99,54
	max	0.060099	0.037205	38.09
	mean	0.033701	0.014088	58.20
	RMS	0.036620	0,018715	48,89
Block Mesh	min	0.0	0.0	0.0
	max	0.019153	0.014321	25.23
	mean	0.002397	0.001820	24.07
	RMS	0.003855	0.002840	26.34
Horse Mesh	min	0.0	0.0	0.0
	max	0.004596	0.003873	15.74
	mean	0.000126	0.000047	62.50
	RMS	0.000205	0.000107	48.08
Bunny Mesh	min	0.0	0.0	0.0
	max	0.003321	0.002761	16.85
	mean	0.000220	0.000096	56.36
	RMS	0.000324	0.000160	50.62

6   Conclusion and discussion

We have presented a method to carry out transformations between triangulations and simplex meshes, and vice versa. Our method is straightforward and does not use iterations. It is based on the interpolation of the initial mesh to find the corresponding vertices of the dual mesh. The interpolation is based on a direct and local minimization of the distance to tangent planes, and points of each face. Our transformation technique was compared to the most frequently used method, which is based on placing the dual points in the center of mass of the initial faces, and the weaknesses of this latter have been illustrated. The performance of the proposed method was measured using a point-to-point distance between both triangulations and simplex meshes, after performing a chain of transformation. Moreover, we measured the Hausdorff distance between meshes after performing a cycle of transformations, *i.e.* after carrying out a transformation to simplex mesh and back to triangulation. The performance of our method was more than satisfactory, providing a more than significant reduction of the error, of nearly 50%. Thus, our method has proven to be adequate to be used in any application requiring topological mesh transformation while preserving geometry, and without increasing complexity.
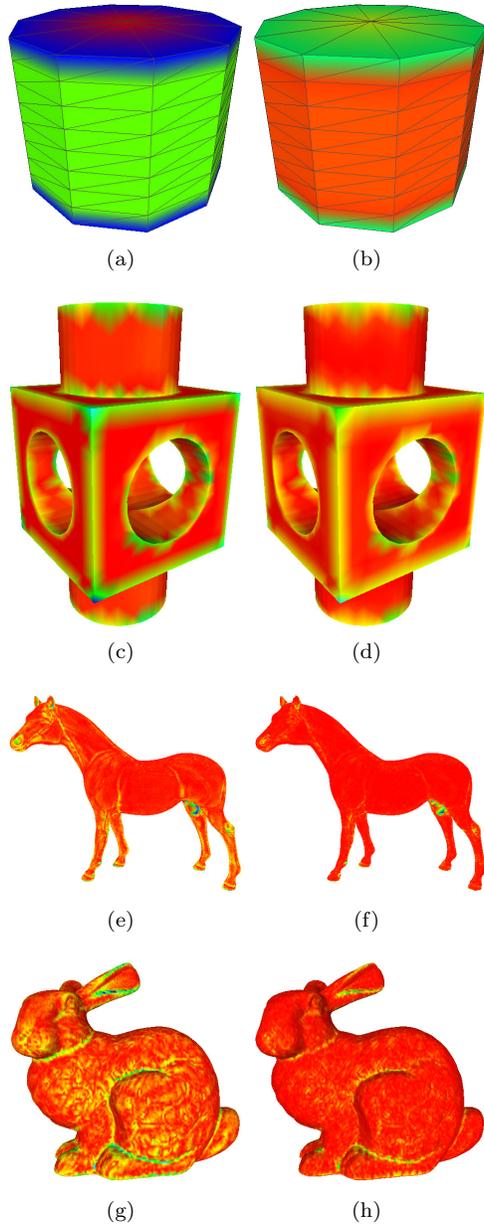
Figure 8: *Prism*, *Block*, *Horse* and *Bunny* meshes colored according to the Hausdorff distance after a cycle of transformations. 1) Left, subfigures a), c), e) and g) using *Center of Mass*. 2) Right, subfigures b), d), f) and h) using our method based on *Distance to the tangent planes*.
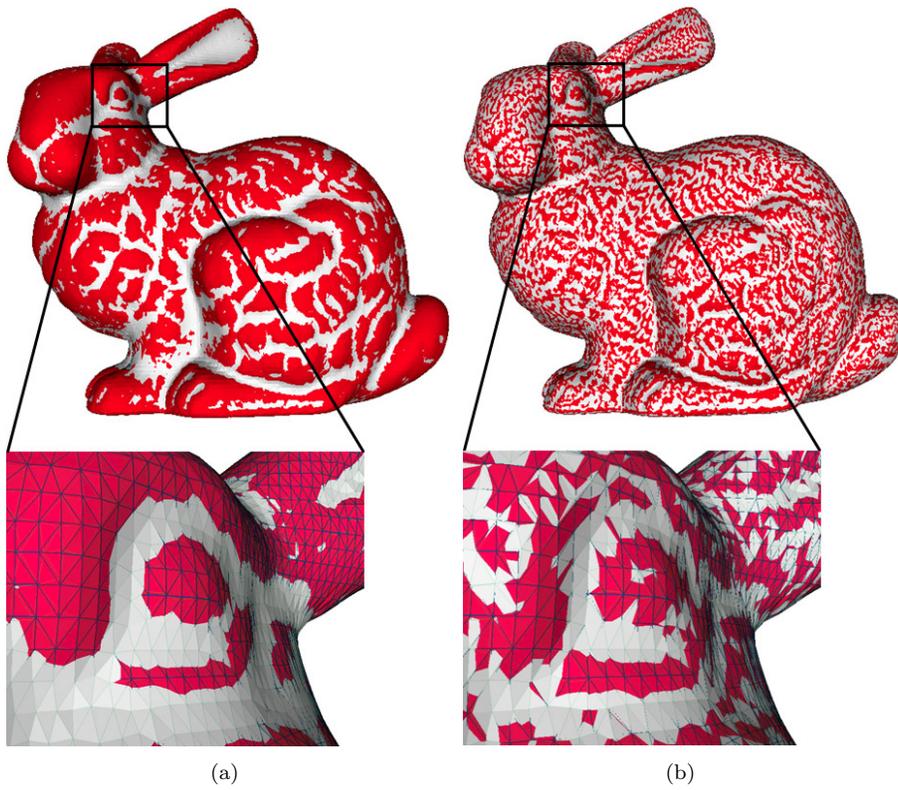
Figure 9: Comparison between the *bunny* original mesh (darker) and after a cycle of transformations (lighter). (a) Using *Center of Mass*. (b) Using our distance to the tangent planes.

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